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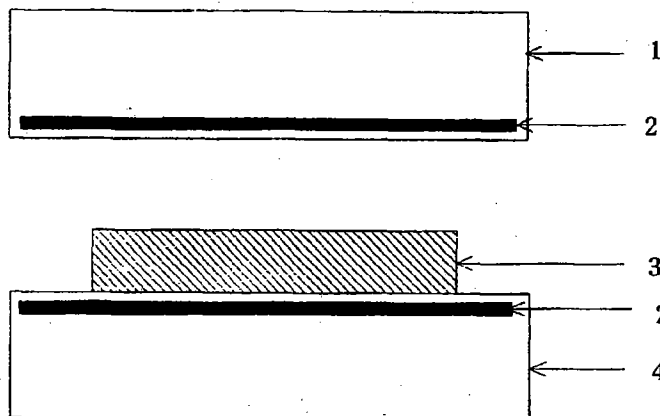
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(54) Title: VACUUM INSULATOR USING GLASS WHITE WOOL AND ITS FABRICATION METHOD



(57) Abstract: The vacuum insulator in accordance with the present invention comprises glass white wool body which density is 0.1 ~ 0.5g/cm<sup>3</sup> in density and is below 0.0023kcal/mh °C in thermal conductivity, and a non permeable container surrounding the body in which the pressure is between 10<sup>-6</sup> ~ 10<sup>-1</sup> torr. The vacuum insulator is fabricated by piling up glass white wool, thermal-pressurizing the piled glass white wool to form a body of 0.1 ~ 0.5g/cm<sup>3</sup> in density wherein the pressurizing is done at 0.007 ~ 1.5kg/cm<sup>2</sup> and under 20 °C for more than 10 minutes, putting the body in the non-permeable container, and producing a vacuum in the container.

WO 01/85445 A1

**VACUUM INSULATOR USING GLASS WHITE WOOL AND ITS  
FABRICATION METHOD**

**TECHNICAL FIELD**

5           The present invention relates to a vacuum insulator which can be used  
as for an insulating and thermal insulating refrigerating/freezing,  
transportation means, and various industrial equipment, And particularly,  
to a vacuum insulator using glass white wool and its fabrication method which  
is pressure forming the glass white wool including no organic or inorganic  
10 binder and air evacuating the white glass wool inside a resistant for  
permeable container.

**BACKGROUND ART**

Conventionally, a polyurethane foam which is foamed using HCFC  
15 such as Freon was mainly used for an insulator, however, a new heat  
insulating system is required recently because a heat insulating function is  
reduced by deterioration when it is used for a long time and using of the  
HCFC is restricted because of environmental problems. In addition, a vacuum  
heat insulating system is searched in order to improve insulating  
20 characteristics of products such as a refrigerator or a freezer.

The vacuum insulating system is a system for minimizing heat transfer  
and maintaining heat insulation by maintaining inside the system to be  
vacuum. In order to maintain the vacuum as a panel state, important elements  
are strength and air pore state of a main body, and heat insulating function

by which the atmosphere pressure can be endured.

The main body used in the vacuum heat insulating system can be made using inorganic materials such as silica powder, fiberglass, molded body of calcium silicate, and using organic materials such as polyurethane and polystyrene foam of fine open cell structure.

Methods of using the silica powder as the main body of the vacuum insulator are disclosed in US Patents Number 4,195,395, 4,425,413, and 4,681,788, a method using the polyurethane foam of open cell structure is disclosed in US Patent Number 4,668,555, and a method of using the polystyrene foam is disclosed in Korean Patent Application No. 95-48619. In addition, there is disclosed a method of increasing insulation function by changing the air pore structure of the polystyrene and polyurethane foam into an anisotropic structure in Korean Patent Laid-open No.1999-010954. The heat insulating performance of the vacuum insulator made by the insulating main body like above is 0.004~0.007 Kcal/mh°C which is better than 0.02 Kcal/mh°C of the polyurethane foam in conventional refrigerator, however, it has lower performance than 0.002~0.003 Kcal/mh°C of the vacuum insulator made using the fiberglass.

The vacuum insulator using the fiberglass is disclosed in US Patent No. 5,090,981, 5,094,899, and 5,330,816.

According to the above US patents, the fiberglass should be molded as a certain form in order to be used as the vacuum insulator, and therefore methods of using small amount of organic or inorganic binder, or compression heat hardening the fiberglass not including the binder are used. In case of

using organic or inorganic binder, the binder may occupy the air pore layer of the fiberglass, or the deterioration is generated, whereby the vacuum insulating effect is reduced and producing cost can be increased because of increasing processes and materials. According to the method of heat  
5 hardening, the fiberglass is compressed in a temperature range of higher than strain point and lower than softening point of the glass constituting the fiber glass, and equilibrium time is maintained, whereby a fiberglass board is made. However, according to this method, the fiberglass should be heated to the temperature higher than the strain point of the glass constituting the  
10 fiberglass, and sealing should be made in a vacuum chamber when vacuum air evacuating, and therefore many processes and energy are required and producing cost is increased.

### **DETAILED DESCRIPTION OF THE INVENTION**

15 Therefore, it is an object of the present invention to provide a vacuum insulator by which production cost and processes can be reduced while maintaining same insulating performance as that of the conventional art using the conventional fiberglass, and therefore productivity is increased.

To achieve the object of the present invention, there is provided a  
20 vacuum insulator using glass white wool comprising a glass white wool body which is  $0.1\sim 0.5\text{g/cm}^3$  in density and is below  $0.0023\text{ Kcal/mh}^\circ\text{C}$  in thermal conductivity and a non permeable container surrounding the body in which vacuum pressure is  $10^{-6}\sim 10^{-1}$  torr.

Also, the vacuum insulator is fabricated by piling up glass white wool

including no organic or inorganic binder, thermal-pressurizing the piled glass white wool to form a body of  $0.1\sim 0.5\text{g/cm}^3$  in density wherein the pressurizing is done at  $0.007\sim 1.5\text{kg/cm}^3$  and under  $20^\circ$  above the strain point of the glass white wool for more than 10 minutes, putting the body in the non permeable container and producing a vacuum in the container.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

Figure 1a through 1d are process charts showing processes of fabricating a vacuum insulator using glass white wool, Figure 1a is showing a process of piling the glass white wool on a lower pressing plate of a press, Figure 1b is showing a process of pressing the piled glass white wool, and Figure 1d is showing a process of vacuum evacuating the glass white wool body in a non permeable container;

Figure 2 is a graph showing thickness change of the piled glass white wool while maintaining the glass white wool body when the piled glass white wool is pressed for 30 minutes under pressure of  $0.007\text{kg/cm}^2$ ; and

Figure 3 is a graph showing change of time by which the thickness of the body can be maintained when the piled glass white wool is pressed under pressure of  $0.007\text{ kg/cm}^3$  and  $400^\circ\text{C}$  temperature.

### **MODE FOR CARRYING OUT THE PREFERRED EMBODIMENTS**

The present invention will now be described with reference to accompanying drawings.

Inventors of the present invention paid attention to a fact that a

diameter of glass of white wool state including no binder is  $10\mu\text{m}$  or smaller than that, and found that the glass can be distorted by pressurizing in lower temperature than strain point of fiberglass having same constitution as the glass.

5           The fabricating method of the vacuum insulator according to the present invention will be described as follows with reference to Figures. Figure 1a through 1d are process charts showing processes of fabricating the vacuum insulator using the glass white wool according to the present invention. Referring to Figures, temperature is maintained to be under  $20^{\circ}\text{C}$   
10   above the strain point of the glass white wool by heating a heating unit 2 on an upper pressing plate 1 and on a lower pressing plate 4. And then, glass white wool 3a of a certain shape including no organic or inorganic binder is piled on the lower pressing plate 4 (Fig.1). The piled glass white wool 3a is pressed by lifting up the lower pressing plate 4(Fig.2). At that time, pressing  
15   temperature, pressing time, and molding pressure are important, and appropriate range will be described later. When the molding is completed, the lower pressing plate 4 is lowered and the glass white wool body 3b is cooled down out of the press(Fig.1c). After that, the glass white wool 3b is put into a non permeable container made using stainless steel thin plates 5 and 6, and  
20   decompressed by vacuum evacuating(Fig.1d) in order to improve the heat insulating function of the glass white wool body 3d. The non permeable container is made using stainless steel thin plate having thickness smaller than  $120\mu\text{m}$ . Through the above depressing processes, the inner structure of the glass white wool body 3d is changed into a structure having greater

heat insulating function. Before the glass white wool body is put into the container, it may be cut its edges or fabricated to be appropriate size. In order to evacuate, a small pipe 7 is connected to one side of the non permeable container and evacuation is made through the pipe 7, and therefore the glass  
5 white wool body 3d inside the container becomes vacuum state. After that, the container is sealed by pressing the pipe 7. It is desirable that the pressure of the non permeable container is between  $10^{-6}$ ~ $10^{-1}$  torr, and the pipe is pressed by a certain amount of load.

The thickness of the glass white wool is searched while changing the  
10 pressing temperature and the pressing time under a certain pressure, in order to set an optimum ranges of temperature and time.

Figure 2 is showing thickness change of the glass white wool body when the piled glass white wool is pressed for 30 minutes under pressure of  $0.007\text{kg/cm}^3$  as maintaining the body. As shown in Figure 2, the thickness for  
15 maintaining the body can be made if the temperature does not reach to a certain level under a certain pressure. In that case, it can be used as the main body of the vacuum insulator. The temperature by which the thickness as the body can be maintained should be  $400^{\circ}\text{C}$  or more which is  $110^{\circ}\text{C}$  below the strain point of the glass white wool. Therefore, the lowest molding  
20 temperature should be larger than the temperature of  $110^{\circ}\text{C}$  below the strain point. However, it is desirable that the highest molding temperature is under  $20^{\circ}\text{C}$  above the strain point in consideration of distortion of the glass white wool.

Figure 3 is a graph showing change of time of maintaining the

thickness as a molded body when the piled glass white wool is pressed in 400°C temperature and 0.007kg/cm<sup>3</sup> pressure. The thickness as the molded body is not made if it is heated for less than 10 minutes, then the molded body is expanded again and it is not suitable to be the main body. Therefore, the pressing time should be more than 10 minutes.

Referring to the above results, the molding condition for maintaining the glass white wool is that the temperature should be higher than 400°C which is about 110°C below the strain point of the glass constituting the glass white wool, the pressure is between 0.007~1.5kg/cm<sup>2</sup>, and that the glass white wool should be pressed more than 10 minutes. If the pressure is larger than the above lowest pressure, the molding by pressing can be made. And if the molding pressure is larger than the above highest pressure, the fiber in the glass white wool is excessively broken, and therefore it can be used as the main body of the vacuum insulator and the insulating performance may be reduced even if the thickness is maintained.

The thermal conductivity of the vacuum insulator fabricated according to the present invention is about 0.002kcal/mh°C, and it is superior to those of the vacuum insulator using the organic or inorganic materials, and calcium silicate body.

The present invention will be described in more detail with reference to embodiments of the present invention, however the present invention is not limited to the embodiments, and various changes and modifications can be made.

#### Embodiment 1.



Glass white wool of about 8~12 $\mu$ m diameters in average including no organic or inorganic binder is used. Borosilicate including B<sub>2</sub>O<sub>3</sub> about 4~5 wt% is included in the glass white wool, the strain point of the glass white wool is 510°C, and an annealing point of the glass white wool is 550°C. The above

5 glass white wool of 200g which is cut the width and length to be 20~30cm is piled on the lower pressing plate of the press. Temperature of the heating unit on the upper and lower pressing plates is maintained to be about 400°C which is 100°C below the strain point. This temperature is the lowest temperature at which the glass white wool body can be maintained. The glass

10 white wool is pressed so that the thickness is to be 2cm by lifting up the lower pressing plate with 450kg load, and is maintained for 30 minutes. After that, the glass white wool is cooled down out of the press by lowering the lower pressing plate. The molded body is fabricated so that the width and the length are respectively to be 20cm, is put into a non permeable container made

15 using stainless steel thin plate of 80 $\mu$ m thickness, and is evacuated to be  $5.6 \times 10^{-5}$  torr through the pipe 7 disposed on side surface of the container. After that, the pipe is pressed and adhered by load of 250kg, and whereby a vacuum insulating panel is fabricated. The thermal conductivity of the vacuum insulating panel measured with the thermal conductivity detector(model

20 Rapid-k, DYNATECH R/D Co.) in the temperature of 20°C in average is 0.0023kcal/mh°C.

#### Embodiment 2.

A vacuum insulating panel is fabricated by the same method as in

Embodiment 1, except that the pressing load is 200kg when the glass white wool is molded.

Embodiment 3.

- 5 A vacuum insulating panel is fabricated by the same method as in Embodiment 1, except that the pressing load is 300kg when the glass white wool is molded.

Thermal conductivity of the vacuum insulators using glass white wool fabricated in Embodiments 1 through 3 are shown in following table 1.

10

Table 1. thermal conductivity of the vacuum insulating panels according to the present invention.

embodiment	Thermal conductivity (kcal/mh°C)	Pressure (torr)
1	0.0023	$5.6 \times 10^{-5}$
2	0.0022	$5.6 \times 10^{-5}$
3	0.0022	$5.6 \times 10^{-5}$

### INDUSTRIAL APPLICABILITY

- 15 As so far described, the vacuum insulating panel using glass white wool and fabricating method according to the present invention has higher heat insulating function than that of conventional vacuum insulating panel using organic materials, in organic material powder, and calcium silicate body, and the high production cost which is a disadvantage of the conventional

vacuum insulating panel using fiberglass as the main body can be reduced,  
whereby the productivity can be greatly increased.

### CLAIMS

1. a vacuum insulator using glass white wool comprising:  
a glass white wool molded body which is  $0.1\sim0.5\text{g/cm}^3$  in density, and  
is below  $0.0023\text{kcal/mh}^\circ\text{C}$  in thermal conductivity; and  
5 a non permeable container surrounding the molded body in which  
pressure is between  $10^{-6}\sim10^{-1}$  torr.
2. A fabrication method of the vacuum insulator using glass white  
wool comprising the steps of:  
10 piling glass white wool including no organic or inorganic binder to be  
a certain shape;  
molding the piled glass white wool by heating and pressing it in a  
temperature under  $20^\circ\text{C}$  above strain point of the glass white wool, under  
pressure between  $0.007\sim1.5\text{kg/cm}^2$ , for more than 10 minutes; and  
15 decompressing the molded glass white wool by putting it into the non  
permeable container and evacuating.
3. The method of claim 2, wherein the lowest molding temperature  
is higher than a temperature which is  $110^\circ\text{C}$  below the strain point of the glass  
20 white wool in the step of molding the glass white wool.
4. The method of claim 2, wherein a density of the molded glass  
white wool is between  $0.1\sim0.5\text{g/cm}^3$ .

5. The method of claim 2 further comprising a step of fabricating edges of the glass white wool body before putting the body into the non permeable container.

5 6. The method of claim 2, wherein the non permeable containers made using stainless steel thin plate having thickness less than 120 $\mu$ m.

7. The method of claim 2, wherein a pipe for evacuating is disposed on one side surface of the non permeable container.

10

8. The method of claim 7 further comprising a step of sealing the pipe by pressing after the step of evacuating the glass white wool in the non permeable container.

15 9. The method of claim 2, wherein the pressure is to be between  $10^{-6}$ ~ $10^{-1}$  torr in the step of evacuating the glass white wool in the non permeable container.

1/3

FIG 1A

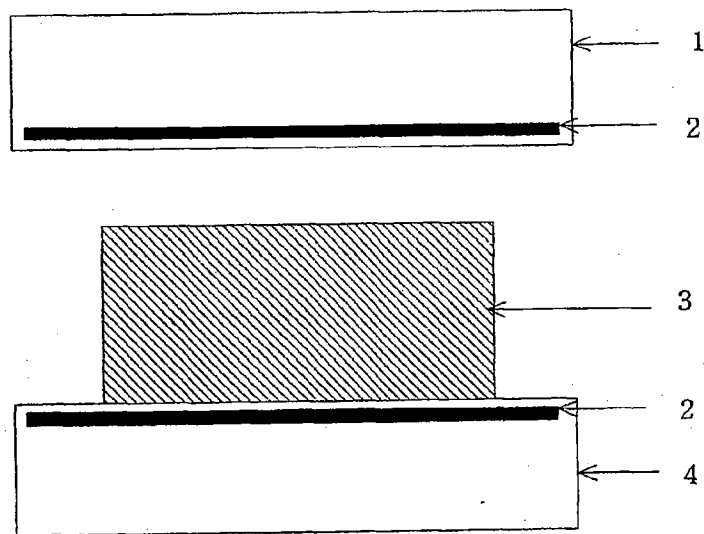
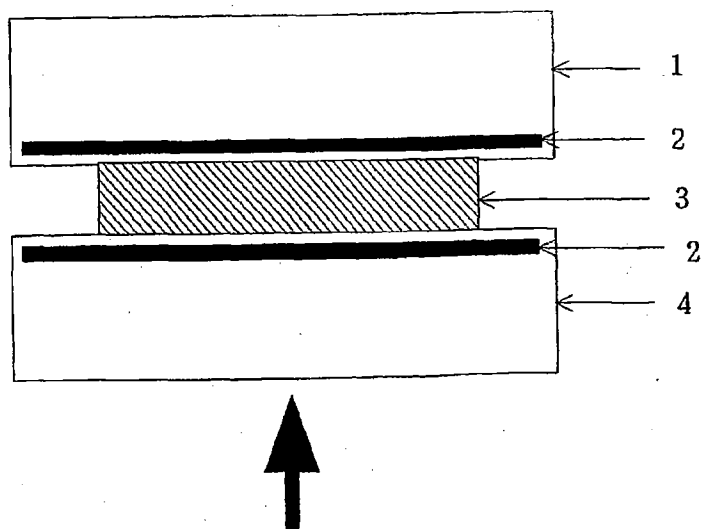


FIG 1B



2/3

FIG 1C

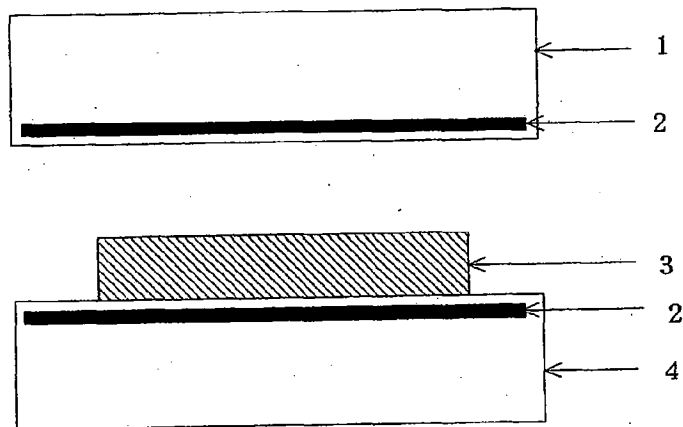
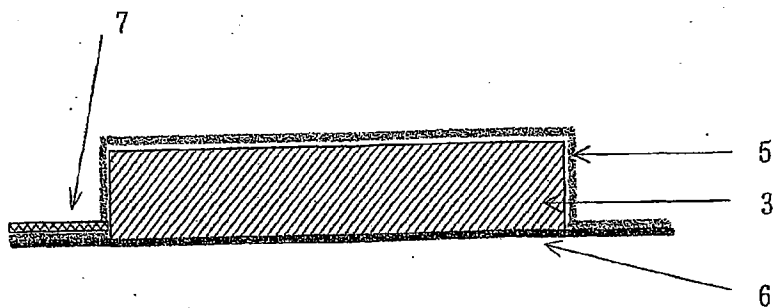


FIG 1D



3/3

FIG 2

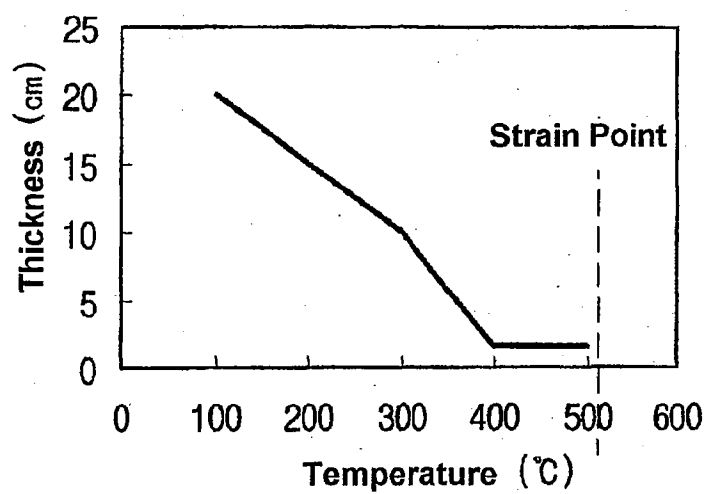
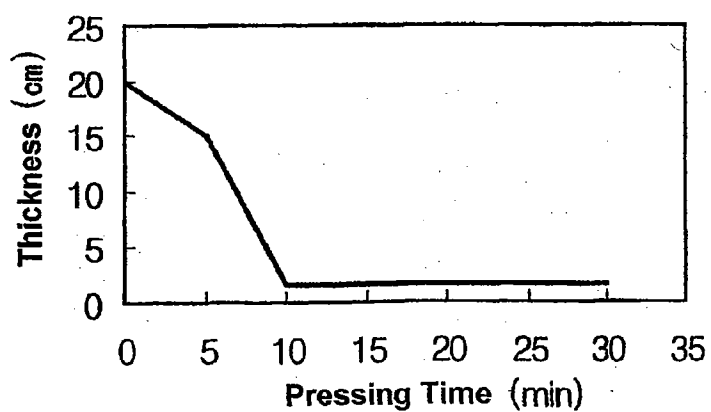


FIG 3





## INTERNATIONAL SEARCH REPORT

International application No.

PCT/KR01/00421

<b>A. CLASSIFICATION OF SUBJECT MATTER</b>		
IPC7 B32B 17/00, C03B 37/06		
According to International Patent Classification (IPC) or to both national classification and IPC		
<b>B. FIELDS SEARCHED</b>		
Minimum documentation searched (classification system followed by classification symbols)		
IPC7 B32B 17/00, C03B 37/06		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)		
<b>C. DOCUMENTS CONSIDERED TO BE RELEVANT</b>		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5094899 B (OWENS-CORNING FIBERGLAS CORP.), 10.MARCH.1992. SEE THE WHOLE DOCUMENT.	1-9
A	US5090981 B (OWENS-CORNING FIBERGLAS CORP.), 25 FEB. 1992. SEE THE COLUMN 3-6.	1-9
A	US 5330816 B (OWENS-CORNING FIBERGLAS TECHNOLOGY INC.), 19. JUL. 1994 SEE THE WHOLE DOCUMENT.	1-9
<input type="checkbox"/> Further documents are listed in the continuation of Box C. <input checked="" type="checkbox"/> See patent family annex.		
<p>* Special categories of cited documents:</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier application or patent but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&amp;" document member of the same patent family</p>		
Date of the actual completion of the international search		Date of mailing of the international search report
16 JULY 2001 (16.07.2001)		18 JULY 2001 (18.07.2001)
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# INTERNATIONAL SEARCH REPORT

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Information on patent family members

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 5094899	10.MARCH.1992.	NONE	
US5090981	25. FEB. 1992.	NONE	
US 5330816	19. JUL. 1994	NONE	

Form PCT/ISA/210 (patent family annex) (July 1998)